

Instructions: items in **black** are graded, items in **gray** are for information only

<p>EX1</p>	<p>4,5 pts</p>
<p>1.1</p> <p>I \Rightarrow C since the derivative of $y = \sqrt{ax}$ at 0 tends to infinity \Rightarrow vertical tangent at O J \Rightarrow A since the derivative of $y = \frac{x^2}{a}$ at 0 tends to 0 \Rightarrow horizontal tangent at O K \Rightarrow B trivial since it is the line $y = x$</p>	<p>Total: 0,5 pt or 0</p>
<p>1.2</p> <p>$I' = \int_{y=0}^a \int_{x=0}^{\frac{y^2}{a}} dx dy$ $J' = \int_{y=0}^a \int_{x=0}^{\sqrt{ax}} dx dy$ $K' = \int_{y=0}^a \int_{x=0}^y dx dy$</p>	<p>Total: 1,5pt</p> <p>0,5 : 0,5 : 0,5</p>
<p>1.3</p> <p>$I = \int_0^a (a - \sqrt{ax}) dx = \left[ax - \frac{2}{3a} (ax)^{\frac{3}{2}} \right]_0^a = \frac{a^2}{3}$ or as normal in y: $I' = \int_{y=0}^a \frac{y^2}{a} dy = \frac{1}{3} [y^3]_0^a = \frac{a^3}{3}$</p> <p>$J = \int_{x=0}^a \left(a - \frac{x^2}{a} \right) dx = \left[ax - \frac{x^3}{3a} \right]_0^a = \frac{2a^2}{3}$ or as normal in y: $J' = \int_{y=0}^a \sqrt{ay} dy = \left[\frac{2}{3a} (ay)^{\frac{3}{2}} \right]_0^a = \frac{2a^2}{3}$</p> <p>$K = \int_{x=0}^a (a - x) dx = \left[ax - \frac{x^2}{2} \right]_0^a = \frac{a^2}{2}$ or as normal in y: $K' = \int_{y=0}^a y dy = \frac{a^2}{2}$</p>	<p>Total: 2,5pt</p>

EX2	6pts+1bonus
<p>2.1</p> <p>Mass of the cylinder: $m_c = \rho\pi R^2 H \sim 3.1\text{g}$ (π g tolerated)</p> <p>Mass of the cone: $m_\Delta = \rho \frac{\pi R'^2 H'}{3} \sim 50\text{g}$ (16π g tolerated)</p>	<p>Total: 1pt</p> <p>0,5</p> <p>0,5</p> <p>(0,25 instead of 0,5 if no units)</p>
<p>2.2</p> <p>Oz is the axis of revolution of the cylinder (ρ does not depend on θ), so G_C is on Oz and the perpendicular plane cutting the cylinder in two halves is a symmetry plane (ρ does not depend on the height) so G_C is at the middle of the cylinder: $G_C(0,0, H' + H/2)$</p>	<p>Total: 1pt</p> <p>0,5+0,5</p> <p>(0 if not justified)</p>
<p>2.3</p> <p>Oz is the axis of revolution of the cone, so G_Δ is on Oz: $G_\Delta(0,0, z_\Delta)$</p> <p>In cylindrical coordinates: $r_\Delta = 0, \theta_\Delta = 0$ leaving us with only z_Δ to be determined.</p> <p>We have $dM = \rho dV = \rho r dr d\theta dz$</p> <p>The variables r and z are connected through the expression: $\frac{R'}{H'} = \frac{r}{z}$, hence we can express, for example, r as a function of z</p> $M_{\Delta z_\Delta} = \int_{z=0}^{H'} \int_{r=0}^{\frac{R'}{H'}z} \int_{\theta=0}^{2\pi} z \cdot \rho r dr d\theta dz$ $= 2\pi\rho \int_{z=0}^{H'} \int_{r=0}^{\frac{R'}{H'}z} z \cdot r dr dz = \pi\rho \int_{z=0}^{H'} [r^2]_{r=0}^{\frac{R'}{H'}z} z dz$ $= \pi\rho \frac{R'^2}{H'^2} \int_{z=0}^{H'} z^3 dz = \pi\rho \frac{R'^2}{4H'^2} H'^4 = \pi\rho \frac{R'^2 H'^2}{4}$ <p>With the mass of the cone found in 2.1 we have: $z_\Delta = \frac{3}{4} H' \sim 2.2\text{cm}$</p> <p>Bonus: $H' > z_\Delta > H'/2$ which makes sense !</p>	<p>Total: 3pt + 0,5 bonus</p> <p>-not counted if already counted in the previous question (0,5 if point not given above)</p> <p>0,5</p> <p>1 (pose the integral)</p> <p>1 (resolution)</p> <p>0,5 (solution)</p> <p>Bonus 0,5 for the comment (in literal or numerical)</p>

<p>2.4</p> <p>For the overall center of gravity we will use the formula of the barycenter: $(M_{\Delta} + M_C) \vec{OG} = M_C \vec{OG}_C + M_{\Delta} \vec{OG}_{\Delta}$</p> <p>from where we take the z-coordinate:</p> $(M_{\Delta} + M_C) z_G = M_C z_C + M_{\Delta} z_{\Delta} \Rightarrow z_G = \frac{M_C z_C + M_{\Delta} z_{\Delta}}{M_{\Delta} + M_C}$ <p>N.A. $z_G = \frac{79}{34} \text{ cm} \sim 2,3 \text{ cm}$</p> <p>Bonus : $M_C \ll M_{\Delta}$ so $z_G \sim z_{\Delta}$ (or if the previous bonus was not given: any comment on the fact that the value 2,3cm “looks nice” or “makes sense”)</p>	<p>Total: 1pt + 0,5 bonus</p> <p>0,25</p> <p>0,5</p> <p>0,5 (no units no points)</p> <p>Bonus 0,5</p>
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<p>EX3</p>	<p>5,5 pts +0,5 bonus</p>
<p>3.1</p> <p>Mass: $M = \iiint_V dM = \iiint_V \rho dV = \iiint_V k \frac{a^2 + r^2}{4a + z} r d\theta dr dz$</p> <p>The bounds of the integral are independent and the function to integrate can be expressed as a product of type $f(r) \cdot g(\theta) \cdot h(z)$ hence we can apply Fubini, writing it as a product of integrals:</p> $M = k \int_0^{2\pi} d\theta \cdot \int_0^a r(a^2 + r^2) dr \cdot \int_{-2a}^{2a} \frac{1}{4a + z} dz$ $M = k \cdot 2\pi \cdot \left[\frac{a^2}{2} r^2 + \frac{1}{4} r^4 \right]_0^a \cdot [\ln(4a + z)]_{-2a}^{2a}$ $M = 2\pi k \left(\frac{a^4}{2} + \frac{a^4}{4} \right) \ln(3)$ $M = \pi k \frac{3a^4}{2} \ln(3)$ <p>Bonus : dimensions are correct (no dimension in the ln and $[k]=ML^{-4}$)</p>	<p>Total: 2 pt + 0,5 bonus</p> <p>0,5 (expression)</p> <p>0,5 (for posing correctly the integral with the right bounds)</p> <p>1 (calculation and result)</p> <p>Bonus 0,5</p>
<p>3.2</p> <p>Parametrization of the cylinder in Cartesian coordinates:</p> $C = \{M(x, y, z) \in \mathbb{R}^3 (x^2 + y^2) \leq a^2 \text{ and } -2a \leq z \leq 2a\} \text{ (or any equivalent form)}$	<p>Total: 1pt</p> <p>1</p>
<p>3.3</p> <p>sketch</p> <p>Distance between the point $M(x, y, z)$ and the axis Oy: $r_{Oy} = \sqrt{z^2 + x^2}$</p>	<p>Total: 1pt</p> <p>0,5</p> <p>0,5</p>

<p>3.4 Moment w.r.t. Oy:</p> $J = \iiint_V r_{Oy}^2 dM = \iiint_V r_{Oy}^2 \rho dV = \iiint_V (x^2 + z^2) k \frac{a^2 + (x^2 + z^2)}{4a + z} dx dy dz$ <p>With bounds:</p> $J = k \int_{z=-2a}^{2a} \int_{y=-1}^1 \int_{x=-\sqrt{1-y^2}}^{\sqrt{1-y^2}} (x^2 + z^2) \frac{a^2 + (x^2 + z^2)}{4a + z} dx dy dz$	<p>Total: 1,5pt</p> <p>0,5 (for the moment of inertia correctly posed with r_{Oy} and ρdV)</p> <p>1 (complete integral with bounds)</p>
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Exercise 4	4 pts+0,5 bonus
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<p>4.1</p> $\vec{0} = \frac{M_S}{M_S+M} \vec{O}b + \frac{M}{M_S+M} \vec{O}a \Rightarrow 0 = -\frac{M_S}{M_S+M} b + \frac{M}{M_S+M} a \text{ or any equivalent equation}$ <p>It follows that:</p> $M_S = M \frac{a}{b}$	<p>Total: 1 pt</p> <p>0,50</p> <p>0,50</p>
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<p>4.2</p> <p>The height of the liquid in the tank has cylindrical symmetry, hence, we should use cylindrical coordinates</p> <p>$V_S = \iiint_{(S)} dV$, with the parametrisation of the sphere as such:</p> <p>$\theta \in [0, 2\pi]$, $z \in [-R, h - R]$ (with the reference at the center of the sphere, for a much simpler calculation), $r \in [0, \sqrt{R^2 - z^2}]$, and $dV = r d\theta dr dz$</p> <p>Hence:</p> $V_S = \int_{\theta=0}^{2\pi} \int_{z=-R}^{h-R} \int_{r=0}^{\sqrt{R^2-z^2}} r dr dz d\theta, \text{ which after resolution should give:}$ $V_S = \pi \left(h^2 R - \frac{h^3}{3} + \frac{2}{3} R^3 \right)$	<p>Total: 2,5pt</p> <p>0,25 (0 if other conclusion, even if the integral and the result is correct in the end)</p> <p>4 * 0,25 (For this or any similar <u>good parametrization</u>, and dV)</p> <p>1,25</p>
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<p>4.3</p> $M_S = \rho V_S = \rho \pi \left(R^2 h - \frac{h^3}{3} + \frac{2}{3} R^3 \right)$ <p>Then, from the result in 4.1 it follows that:</p> $\frac{\rho \pi b}{M} \left(R^2 h - \frac{h^3}{3} + \frac{2}{3} R^3 \right) = a$ <p>NB: this is the equation the engineer should program in its computer that controls the pump</p> <p>Bonus: check dimensions either in Q4.2 or Q4.3</p>	<p>Total: 0,5 pt + 0,5 bonus</p> <p>0,25</p> <p>0,25</p> <p>Bonus 0,5</p>
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