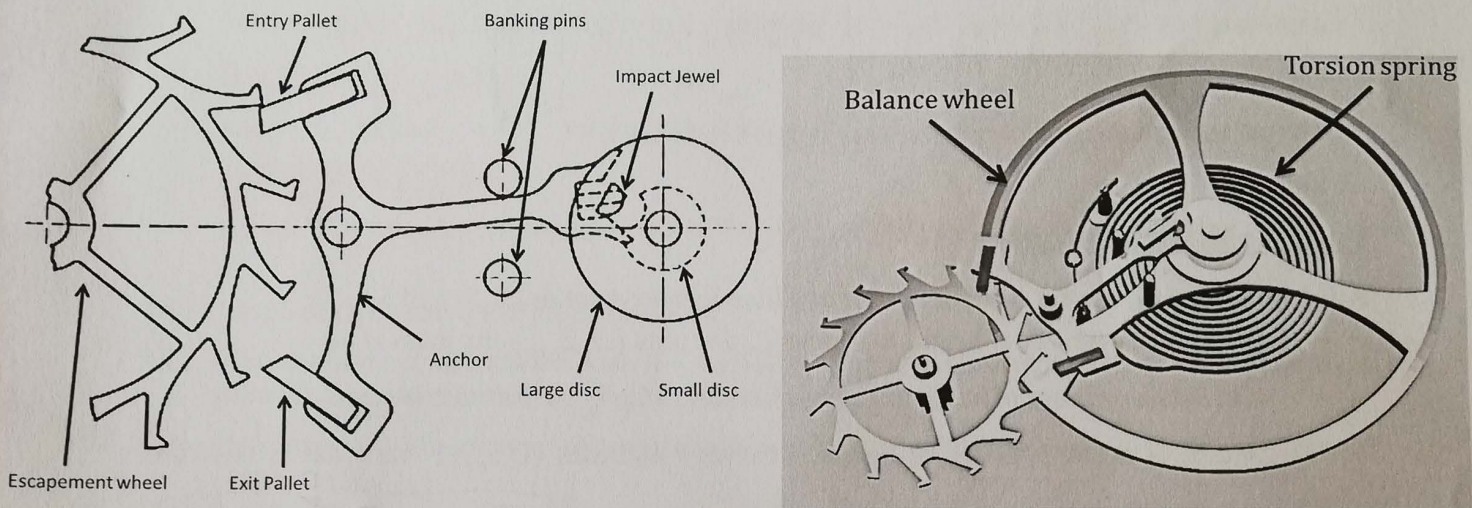


**Mechanics – Test# 4**  
08/04/2019 – 1h30 (10h15 – 11h45)

Authorised documents:

- Personal Formula sheet (3 pages + 1 joint wrench + 1 inertia matrices)
- Non programmable Calculator

**Analysis of a Swiss anchor escapement mechanism**



**Figure 1** – Swiss anchor escapement mechanism of a watch

**System description**

The Swiss anchor escapement mechanism (**Figure 1**) is a key component in many mechanical watches as it controls watch accuracy to a large extent.

This mechanism shown in **Figure 2** is operated by the energy stored in a torsion spring  $R_T$  of stiffness  $k$  (not represented in figure2) which makes solid  $S_1$  oscillate periodically by an angle  $\pm\alpha$  around axis  $(O_1, \vec{z}_0)$  at a frequency of a couple of Hz. Solid  $S_1$  comprises a large disc  $S_A$ , a small disc  $S_B$  and an impact jewel  $S_C$  (**Figure 3**). It is linked to the watch frame  $S_0$  by a revolute joint of axis  $(O_1, \vec{z}_{0,1,2})$  and parameter  $\alpha = (\vec{x}_0, \vec{x}_1) = (\vec{y}_0, \vec{y}_1)$  ;

The  $\pm\alpha$  oscillations of  $S_1$  induce a periodic push of the anchor  $S_2$  by an angle  $\pm\beta$  because of the point contact at  $A$  between the impact jewel  $S_C$  and  $S_2$ . The mechanical actions transmitted by the point contact joint between  $S_1$  (via  $S_C$ ) and  $S_2$  at point  $A$  are expressed by the wrench  $\left\{ F_{2 \rightarrow 1} \right\}_A$ .

The anchor  $S_2$  is linked to the watch frame  $S_0$  by a revolute joint of axis  $(O_2, \vec{z}_0)$  and parameter  $\beta = (\vec{x}_0, \vec{x}_2) = (\vec{y}_0, \vec{y}_2)$ .

The periodic oscillation of anchor  $S_2$  permits releasing the rotation of the escapement wheel  $R_E$  (not modeled) which is in contact with  $S_2$  at point  $D$ . The contact forces at point  $D$  are known and expressed by the wrench  $\left\{ F_{R_E \rightarrow 2} \right\}_D$ .



**Hypotheses :**

- the frame  $R_0 = (O_1, \vec{x}_0, \vec{y}_0, \vec{z}_0)$  is a Galilean frame,
- the problem is considered as planar,
- the gravity is downwards along  $\vec{z}_{0,1,2}$ ,
- all the joints are perfect,
- the torsion spring  $R_T$  acts onto  $S_1$  at point  $O_1$ . It has a constant stiffness  $k$  and its angle at rest is  $\alpha_0$ . Its mass is neglected and its force wrench is denoted  $\left\{ F_{R_T \rightarrow 1} \right\}_{O_1}$ .
- The contact force wrench between  $S_1$  and  $S_2$  at point  $A$  reads:

$$\left\{ F_{2 \rightarrow 1} \right\}_A = \left\{ \begin{array}{l} \vec{R}_{2 \rightarrow 1} = X_{21} \vec{x}_1 + Y_{21} \vec{y}_1 \\ \vec{M}_{2 \rightarrow 1}(A) = \vec{0} \end{array} \right\}_A$$

All the geometrical parameters are defined in figure 2.

**Part 1 : Mass Geometry**

**Solid  $S_1$**  of mass  $m_1$  can be decomposed into 3 homogeneous solids,  $S_A, S_B$  and  $S_C$ :

- solid  $S_A$  is a cylinder of height  $h_A$ , radius  $R_A$  and axis  $(O_1, \vec{z}_{0,1,2})$ . Its mass is  $m_A$ .
- solid  $S_B$  is a cylinder of height  $h$ , radius  $r$  and axis  $(O_1, \vec{z}_{0,1,2})$ . Its mass is  $m_B$ .
- solid  $S_C$  is a half-cylinder of height  $h$ , radius  $r$  and axis  $(C, \vec{z}_{0,1,2})$ . Its mass is  $m_C$ . The

coordinates of the mass center  $G_C$  of solid  $S_C$  are given by:  $\overrightarrow{O_1 G_C} = \left( +L_C + \frac{4R}{3\pi} \right) \vec{y}_1 + \frac{h}{2} \vec{z}_1$ .

**Solid  $S_2$**  has negligible thickness, its mass center is  $G_2$   $\left( \overrightarrow{O_2 G_2} = x_{G_2} \vec{x}_2 \right)$ , its mass is  $m_2$ .

Do not calculate the masses of the solids.

The inertia matrices of  $S_1, S_2$  and  $S_C$  are given as:

$$\overline{I}_{O_1, S_1} = \begin{bmatrix} A_1 & 0 & 0 \\ 0 & B_1 & -D_1 \\ 0 & -D_1 & C_1 \end{bmatrix}_{R_1} \quad \overline{I}_{G_2, S_2} = \begin{bmatrix} A_2 & -F_2 & 0 \\ -F_2 & B_2 & 0 \\ 0 & 0 & C_2 \end{bmatrix}_{R_2} \quad \overline{I}_{G_C, S_C} = \begin{bmatrix} A_{SC} & 0 & 0 \\ 0 & B_{SC} & 0 \\ 0 & 0 & C_{SC} \end{bmatrix}_{R_1}$$

- 1.1 Justify the inertia matrix form of solid  $S_2$  at point  $G_2$  expressed in basis  $R_2$ .
- 1.2 Justify the inertia matrix form of solid  $S_1$  at point  $O_1$  expressed in basis  $R_1$ .
- 1.3 Determine the coordinates of the mass center  $G_1$  of solid  $S_1$  in  $R_1$ , express  $\overrightarrow{O_1 G_1}$ .  
For the next questions, these coordinates will be denoted:  $\overrightarrow{O_1 G_1} = x_{G_1} \vec{x}_1 + y_{G_1} \vec{y}_1 + z_{G_1} \vec{z}_1$

**Study of solid  $S_1 = \{S_A \cup S_B \cup S_C\}$ :**

- 1.4 Determine the inertia matrix of the small disc  $S_B$  at  $O_1$ . Detail the expression of the matrix terms.



For the next questions, one will use Binet's notations for the matrix terms:  $A_{SA}, B_{SA}, C_{SA}, D_{SA}, E_{SA}, F_{SA}$

1.6 Determine the inertia matrix of the impact jewel  $S_C$  at  $O_1$ . Use the terms of  $\bar{I}_{G_C, S_C}$ .

1.7 Determine the inertia matrix of  $S_1$  at  $O_1$ . Detail the expression of the matrix terms.

For the next questions, one will use Binet's notations for the matrix terms:  $A_1, B_1, C_1, D_1, E_1, F_1$

## Part 2 : Kinetics and dynamics

The kinematic scheme of the Swiss escapement anchor mechanism is represented in Figure 2. It is composed of:

- the watch frame  $S_0$  (watch housing),  $R_0 = (O_1, \vec{x}_0, \vec{y}_0, \vec{z}_0)$ ,
- solid  $S_1$  (mass  $m_1$ ) linked to  $S_0$  by a revolute joint of axis  $(O_1, \vec{z}_{0,1,2})$  and parameter  $\alpha = (\vec{x}_0, \vec{x}_1) = (\vec{y}_0, \vec{y}_1)$ ,
- solid  $S_2$  linked to  $S_0$  by a revolute joint of axis  $(O_2, \vec{z}_{0,1,2})$  and parameter  $\beta = (\vec{x}_0, \vec{x}_2) = (\vec{y}_0, \vec{y}_2)$ ,
- a torsion spring  $R_T$  (not represented in Figure 2), of stiffness  $k$ , acting on  $S_1$ .

2.1 Graph of links, change of basis diagrams.

2.2 Give the wrench associated with the torsion spring  $R_T$  mechanical actions onto solid  $S_1$  at point  $O_1$  expressed in the coordinate system  $R_1$ .

2.3 Determine the kinetic wrench (momentum wrench) of solid  $S_1$  at point  $O_1$  in its motion with respect to  $R_0$ .

2.4 Determine the dynamic wrench of solid  $S_1$  at point  $O_1$  in its motion with respect to  $R_0$ .

2.5 Write the dynamic sum theorem for solid  $S_1$ .

2.6 Write the dynamic moment theorem applied to solid  $S_1$  at  $O_1$

2.7 Determine the dynamic wrench of solid  $S_2$  at point  $O_2$  in its motion with respect to  $R_0$ .



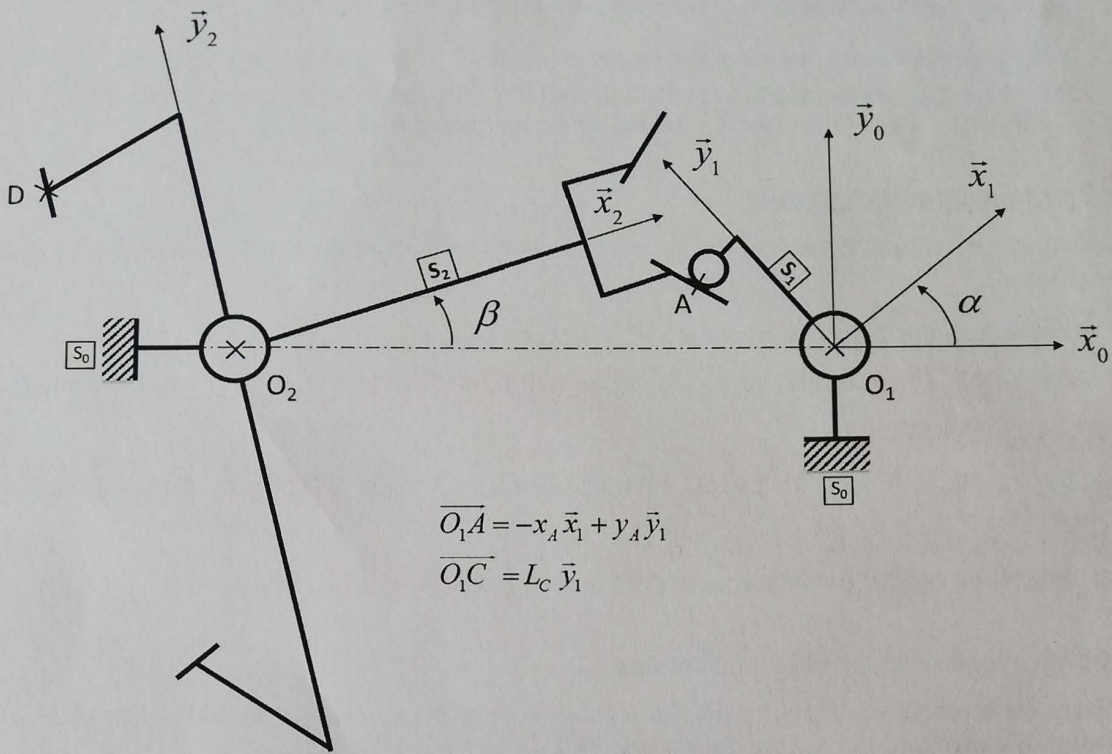


Figure 2 : Schematic representation of  $S_1$  and  $S_2$

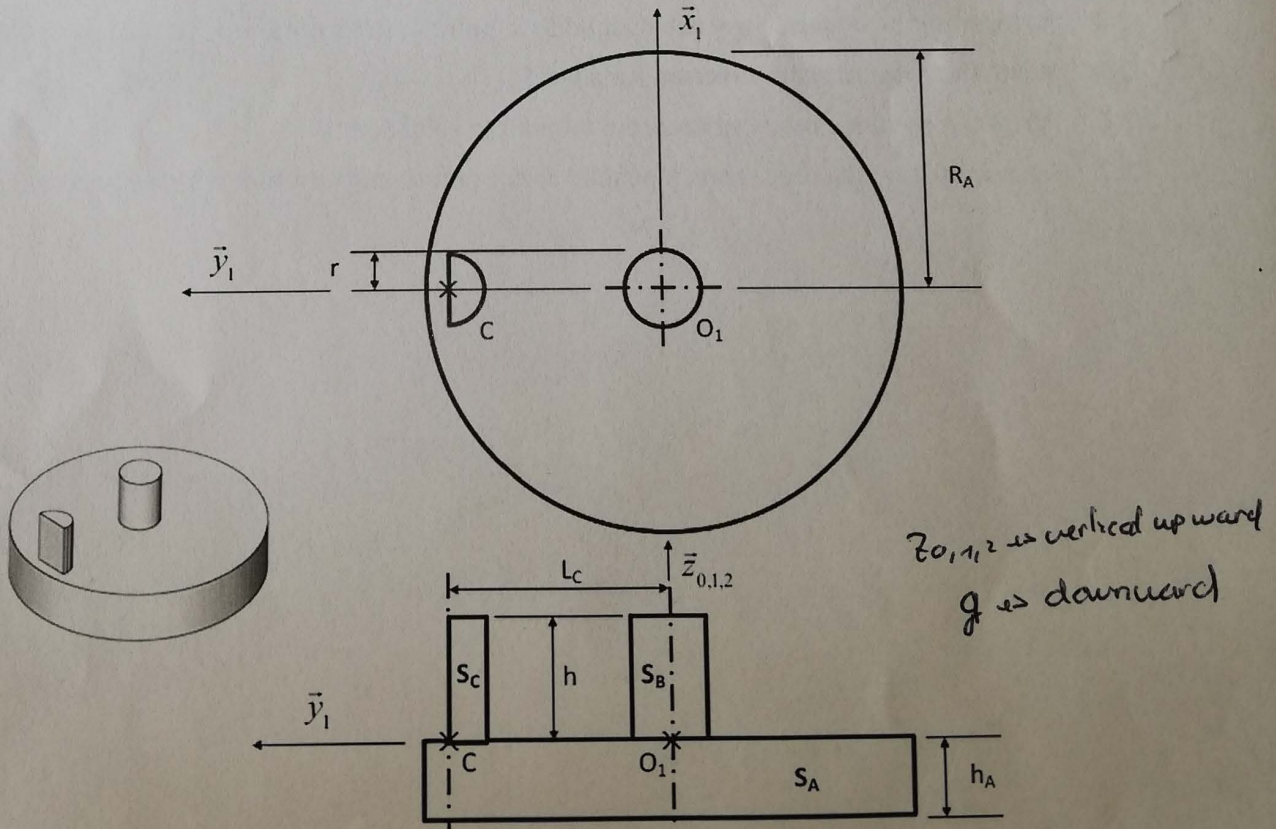


Figure 3 : Solid  $S_1 = \{S_A \cup S_B \cup S_C\}$