## Instructions:

Present your answers clearly and legibly. Calculator (any type but not internet connected) and 3-pages formulary permitted. Any illogical results, without comment, will be further penalized.

## Part 1

## The MOS Transistor

Metal-Oxyde-Semiconductors (MOS) transistors represent the most fundamental component of micro-nanoelectronics. Millions of them are necessary to build an electronic memory, however they are all made according to the same structure shown in Fig.1. Their working principle is relatively simple: a conducting channel connecting two conducting areas called "source" and "drain" is created or suppressed in relation with the voltage applied on the grid. A voltage source $V_{D S}$ being applied between source and drain as shown in Fig.1, for a given grid voltage $V_{0}$ the channel doesn't exist and consequently $i_{D S}=0$ whereas for another voltage $V_{1}$ the channel is created and consequently $i_{D S} \neq 0$. In this subject our goal is to study this structure when it is passing, i.e. when the channel between source and drain exists.


Figure 1: Working principle of the MOS transistor
The structure can be roughly modeled by a parallel-plate capacitor having infinitely large plates. This parallel-plate capacitor is made of two infinitely-large electrodes (A) and (B) which are first assumed to be made of metal. A potential difference $U$ is maintained at their terminals as indicated in Fig. 2. Plate (A) represents the channel whereas plate (B) represents the grid. The surface charge density coming up in plate $(\mathrm{A})$ is denoted $\sigma_{\mathrm{A} 0}$ whereas the one coming up in plate $(\mathrm{B})$ is denoted $\sigma_{\mathrm{B} 0}$. At first, the space between the plates is assumed to be filled by air of absolute permittivity $\varepsilon_{0}$ : this situation is shown in Fig.2A. The whole device will be considered equivalent to a capacitor having plates infinitely large when considering symmetries and invariances. We will use the Cartesian coordinate system $\left(\overrightarrow{u_{x}}, \overrightarrow{u_{y}}, \overrightarrow{u_{z}}\right)$ shown in Fig. 2A.

Question 1: Determine rigorously the direction of the electric field $\vec{E}$ existing anywhere in the space between the plates (for $0<z<\mathrm{e}$ ), as well as the variables it depends on.


Figure 2: Modeling of the MOS transistor in conducting state by considering 3 different configurations (see detail in the text). Although the voltage source is present in the 3 configurations, it is only represented in the configuration A for simplicity

Question 2: Prove rigorously that $\sigma_{\mathrm{B} 0}=-\sigma_{\mathrm{A} 0}$.
Question 3: By use of Maxwell's equations in point form (only this method is allowed), calculate the electric field in the space between the plates defined by $0<z<e$ as a function of the data of the exercise and in particular as a function of $\sigma_{\mathrm{A} 0}$.

Question 4: Calculate with a detailed demonstration the capacitance $\mathrm{C}_{0}$ of such a transistor having a surface $S$ as a function of $\varepsilon_{0}, S$ and $e$.

Question 5: Numerical application: calculate $\mathrm{C}_{0}$ if $\mathrm{e}=1.2 \mathrm{~nm}, \mathrm{~S}=2.8 \times 10^{-14} \mathrm{~m}^{2}, \varepsilon_{0}=\frac{1}{36 \pi} 10^{-9} \mathrm{SI}$ which corresponds to a distance between source and drain of 28 nm .

Now, in the space between the plates there is a plane having a surface charge density $\sigma_{z}$ uniform and positive, located parallel to the plates at $\mathrm{z}=\mathrm{e}_{1}$. The surface charge density that comes up now on plate $(\mathrm{A})$ is denoted $\sigma_{\mathrm{A} 1}$ whereas the one coming up on plate $(\mathrm{B})$ is denoted $\sigma_{\mathrm{B} 1}$. This situation corresponds to the one described in Fig. 2B. The permittivity of the space between the plates remains $\varepsilon_{0}$.

Question 6: By using the general form of Gauss' law in its integral form (no other method is allowed) and by taking into account the presence of $\sigma_{\mathrm{z}}$, calculate the electric field in the whole area between the plates. The E-field should be expressed as a function of $\sigma_{\mathrm{Al}}, \sigma_{\mathrm{z}}$ and $\varepsilon_{0}$.

Question 7: Express and verify the boundary conditions at $\mathrm{z}=\mathrm{e}_{1}$ ( 2 boundary conditions are expected).
Question 8: Calculate $\sigma_{A 1}$ as a function of $U, e, \sigma_{z}, e_{1}$ and $\varepsilon_{0}$. Deduce from it the variation of the surface charge density in the plates, $\Delta \sigma=\sigma_{\mathrm{Al}}-\sigma_{\mathrm{A} 0}$ due to the presence of the plane charged with $\sigma_{\mathrm{z}}$.

Question 9: Determine the expression of the potential $\mathrm{V}(\mathrm{z})$ between $\mathrm{z}=0$ and $\mathrm{z}=\mathrm{e}$ and plot $\mathrm{V}(\mathrm{z})$ schematically. To do that, assume that $\mathrm{V}(0)=\mathrm{U}>0$ and that $\mathrm{V}(\mathrm{e})=0$.

Question 10: Bonus: what will be the influence of the presence of a charged plane located in the space between the plates (like $\sigma_{z}$ ) on the current isp?

In real devices, the space between the plates is not filled with air but with a dielectric. Currently this dielectric is a hafnium oxide of absolute permittivity $\varepsilon_{2}$ with possibly traces of nitrogen or silicon: $\mathrm{HfO}_{2}, \mathrm{HfSiO}_{2}$ or HfSiON. The growth of Hafnium oxide on silicon induces several defects at the interface between the two materials. Such defects are detrimental to the performances of the transistor. To reduce the defects, we insert between the silicon and the hafnium oxide a layer of $\mathrm{SiO}_{2}$ of absolute permittivity $\varepsilon_{1}$. The final structure, represented in Fig. 2C, still has a total thickness e. Subsequently,
the thickness of the $\mathrm{SiO}_{2}$ layer being denoted $\mathrm{e}_{1}$ and that of the hafnium oxide $\mathrm{e}_{2}$, we have $\mathrm{e}=\mathrm{e}_{1}+\mathrm{e}_{2}$. In the rest of the exercise, as the charged plane $\sigma_{\mathrm{z}}$ doesn't exist anymore we will denote $\sigma_{\mathrm{A} 2}$ and $\sigma_{\mathrm{B} 2}$ the surface charge densities coming up on the plates (A) and (B).

Question 11: Determine the expression of the new capacitance $C_{1}$ of this structure. Justify imperatively your answer. Compare with the capacitance $\mathrm{C}_{0}$ knowing that the smallest among the permittivities $\varepsilon_{1}$ and $\varepsilon_{2}$ is approximately equal to four times $\varepsilon_{0}$.

The geometry of the channel in working conditions is represented in Fig. 3. When the voltage $V_{S D}$ is applied between source and drain, an electric field $\overrightarrow{E_{S D}}$ assumed to be uniform is created in the direction (Oy):


Figure 3: Channel of the MOS transistor polarized by a voltage $V_{S D}$

$$
\overrightarrow{E_{S D}}=E_{S D y} \cdot \vec{u}_{y} \text {, with } \mathrm{E}_{S D \mathrm{y}}=\mathrm{cst}
$$

The resistivity of the channel in working conditions is not perfectly uniform. It depends on the depth according to the relation:

$$
\rho(z)=\rho_{0}-\alpha z \text { if }-\alpha<z<0 \text { with } \alpha>0
$$

Question 12: Calculate in these conditions the total resistance $R_{c}$ of the channel of thickness $a$ and volume $\tau=a W L$ as a function of $a, \rho_{0}, W, L$ and $\alpha$.

Indications: calculate first the elementary resistance $d R$ of an appropriately chosen part of the channel (mind the orientation of the electric field!). Then the elementary resistances will be put together to build up the total resistance. Please justify all calculations.

If $\rho_{0} \gg \alpha a$ then the resistance $R_{C}$ becomes: $R_{C}=\rho_{0} \cdot \frac{L}{W a}$ (well-known formula corresponding to the case of a rod, homogeneous and with constant cross-section)

Question 13: Numerical application: In the framework of this approximation calculate $R_{C}$ if $\rho_{0}=10^{-4} \Omega . \mathrm{cm}, a=2 \mathrm{~nm}, W=1 \mu \mathrm{~m}, L=28 \mathrm{~nm}$.

## Part II : Synchronous motors

A synchronous motor consists of a stator and a rotor. The stator produces the rotating magnetic field which creates the torque that rotates the rotor. We will first study the principle of the stator.

The stator consists of two identical systems $\left(S_{1}\right)$ and $\left(S_{2}\right)$; one of them, shown in Figure 4, consists of two solenoids of same axis, connected in series so that the current flowing through them has the same orientation. In the case of the system $\left(S_{1}\right)$, the axis of the solenoids is denoted $O x$.


Figure 4: System $\left(S_{1}\right)$, consisting of two solenoids of same axis.

Question 1 : Give (and justify) the direction and orientation of the magnetic field $\vec{B}$, produced by the system ( $S_{1}$ ) at point $O$. (We will neglect in the study of the topography of the $\vec{B}$ field the presence of the cables connecting the 2 solenoids).

At point $O$, equidistant from the two solenoids where a current $i$ is flowing, it will be admitted that the norm of the $\vec{B}$ field is $\|\vec{B}\|=K . i$.

We now place two identical systems $\left(S_{1}\right)$ and $\left(S_{2}\right)$, perpendicular to each other. Each system has an equivalent resistance $R$ and a total inductance $L$ and is part of an electrical circuit shown in Figure 5 (where $R$ is not shown, and $R_{0}$ represents a resistance different from $R$ ). The voltage source delivers a sinusoidal voltage $u(t)=U_{0} \cos \left(\omega_{0} t\right)$. We will use a Cartesian coordinate system ( $\vec{u}_{x}, \vec{u}_{y}, \vec{u}_{z}$ ) defined on Figure 5.


Figure 5: Sketch of the stator constiting of two systems $\left(S_{1}\right)$ and $\left(S_{2}\right)$ perpendicular to each other.
The current $i_{1}$ flowing through $S_{1}$ is of the form $i_{1}(t)=I_{1} \cos \left(\omega_{0} t-\varphi_{1}\right)$, the current $i_{2}$ flowing through $S_{2}$ is of the form $i_{2}(t)=I_{2} \cos \left(\omega_{0} t-\varphi_{2}\right)$.

Question 2 : Express $I_{1}, I_{2}, \varphi_{1}$ and $\varphi_{2}$ as a function of $U_{0}, R, R_{0}, L, C$ and $\omega_{0}$ (a simplified circuit diagram of the device will be drawn beforehand and any mutual induction between the coils will be neglected).

Question 3 : $R, L$, and $\omega_{0}$ being fixed, what value should be given to $C$ to have $I_{1}=I_{2}$ ?
One could further demonstrate that $\varphi_{2}-\varphi_{1}=\frac{\pi}{2}$ when $R_{0}=L \omega_{0}-R$.

## The following questions do not need to have answered the previous questions.

Question 4 : Considering the previous conditions fulfilled $\left(\varphi_{2}-\varphi_{1}=\frac{\pi}{2}, I_{1}=I_{2}\right)$, give the expression of the total field $\vec{B}_{T}$ at point $O$ as a function of $K, \omega_{0}, \varphi_{1}$ and $I_{1}$.

Question 5 : Justify the name of rotating field for the field $\vec{B}_{T}$.
The moving part of the synchronous motor, the rotor, consists here of a frame around which a wire is wound, building up a current loop (of surface $S$ ) equivalent to a magnet, of magnetic moment $\vec{M}$. We will first consider the current in the current loop constant, and so will be the norm $M_{0}$ of $\vec{M}$. The previous $\vec{B}_{T}$ field, which rotates at the speed $\omega_{0}$ (same angular speed as priviously) around the $O z$ axis, is supposed here uniform in the whole region of the rotor. It is further assumed that the rotor, and thus $\vec{M}$, also rotates around the $O z$ axis with an angular velocity $\omega$. The vectors $\vec{B}_{T}$ and $\vec{M}$ thus form between them an angle $\theta(t)$ at any time (see Figure 6).


Figure 6: Relative positions of the $\overrightarrow{B_{T}}$ field and the magnetic moment $\vec{M}$

Question 6 : Knowing that $\theta(0)=\theta_{0}$, express $\theta(t)$ as a function of $\omega, \omega_{0}$ and $\theta_{0}$.
The expression of the torque exerted by the field $\vec{B}_{T}$ on the rotor is given: $\vec{\Gamma}=\vec{M} \wedge \vec{B}$.
Question 7 : Give the expression of $\|\vec{\Gamma}\|$ as a function of $M, B_{T}, \omega, \omega_{0}$ and $\theta_{0}$. Why can the synchronous motor only work for $\omega=\omega_{0}$ ?

Several phenomena prevent this condition ( $\omega=\omega_{0}$ ) from being easily fulfilled. In particular, since the angle varies, which is inevitably the case in the engine start phase, the flux of the magnetic field $\vec{B}_{T}$ through the frame also varies.

Question 8 : Express the variation of the flux as a function of $\theta(t), \dot{\theta}(t)=\frac{d \theta}{d t}, B_{T}$, and $S$ (we will still consider that the rotor is subjected to a uniform field over all its whole section $S$ ).

Question 9 : What will then happen in the rotor current loop? Can we consider, as we did previously, that the current flowing in the rotor is constant? Why?

Question 10 : What can be said about the magnetic moment $\vec{M}$ ? Why does the rotor also affect the stator?
Question 11 : Make a sketch of the electrical circuit equivalent to the rotor knowing that the latter is powered by a generator delivering a voltage $u_{r}(t)$ and that it has a resistance $R_{r}$ and a self-inductance $L_{r}$. Write the electrical equation of this circuit as the function of the data of the text.

To conclude, we see that the synchronous motor is not as simple as it seems and requires a fine control of the current and/or the voltage creating the rotating field and the magnetic moment.

## Part III: Waves

A wave carrying a vector signal $\vec{S}$ is represented by the following equation (with $S_{0}$, and $\delta$ positive constants) :

$$
\vec{S}(x, y, z, t)=S_{y} \vec{u}_{y}=S_{0} e^{-\delta|x|} e^{-\delta|z|} \cos (\omega t-k y) \vec{u}_{y}
$$

Answer the following questions, whose purpose is to describe this wave, justifying imperatively each answer :
Question 1: What is the direction of propagation of the wave?
Question 2 : Is this wave uniform?
Question 3 : What is the direction of polarization of the wave?
Question 4 : Is this wave transversal or longitudinal?
The frequency of the wave is $f=915 \mathrm{MHz}$, its wave number $k=19.8 \mathrm{rad} . \mathrm{m}^{-1}$. We also give: $\delta=8.45 \mathrm{~m}^{-1}$
Question 5 : Calculate the values of the wavelength and of the phase velocity.
Question 6 : Represent schematically (but with sufficient accuracy) the component $S_{y}$ of $\vec{S}$ along the ( Oz ) axis, for $t=\frac{T}{2}$, where $T$ is the period of the wave.

Question 7 : Represent $S_{y}$ as a function of time at point $O(0 ; 0 ; 0)$ and at point $M(0 ; 7.9 \mathrm{~cm} ; 0)$.

